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CONSIDERATIONS OF THE DYNAMIC COMFORT INDICATORS IN VERY EFFICIENT ENERGETIC BUILDINGS

ΒY

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Abstract. Imposition of new energy requirements for future buildings (buildings NZB) requires a revision of the rules on their design parameters or rules on hygro-thermal comfort, adapting them to the changing demands that buildings and their improvement. On the other hand, the strategies to ensure comfort in these buildings must be carefully analyzed as indoor climate or comfort hygro-thermal interior is influenced by external climate, performance building and user requirements. The paper presents an analysis of the impact of climatic variations summer on indicators of comfort in buildings NZBE by evaluating them according to rules SR EN 15251 and ASHRAE -55. The analysis aims to highlight the dynamics indicators comfort in actual operating conditions different from those considered in the design process, and identifying strategies appropriate control.

Keywords: indoor quality environment; dynamics comfort indicators; passive strategy control of indoor quality.

1. Introduction

The notion of comfort is a complex notion, defined synthetically by

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"sensation of well/satisfaction that is felt by human body in relation to its external environment".

Comfort problems related to have been in the last 50 years, the subject of the multiple studies and research designed to establish parameters of necessary comfort to building design. In recent years, the comfort parameters are required to performance evaluation (especially energetically) of the buildings and installations afferent, and to establish strategies to control installations systems.

Quality criteria relating to indoor ambiance aimed hygro-thermal comfort, visual, electro-magnetic, acoustic, health (indoor environmental quality: air emissions, ...; required water ...).

The parameters that characterize the indoor environment are relatively numerous and highly variable over time. Man, as a user of indoor space is influenced by the nature and dynamics of these parameters and, in his turn may contribute to altering the characteristics and dynamics of the environment in which he operates. Consequently there is a need to provide the appropriate parameters to ensure an optimal indoor climate in terms hydro-thermal and healthy for the human being and its activities. By default appears and the need for accurate forecasting of the values required to design the heating/cooling systems that ensure comfort and proper designing their control strategies.

In the current context, European and national, energetic and climatic, is absolutely necessary the reconsider the concept of habitat and the mandatory minimum values for defining the parameters for different levels of hygrothermal comfort for the energy-efficient buildings.

Some of efficient energy buildings are characterized by hyper-tightness and hyper-insulation. These are practically disconnected from the external environment. These buildings require intervention controlled to ensure the hygro-thermal comfort inside. Other energy efficient buildings (some buildings NZBE, passive house, passive solar buildings, bio-climatic buildings, ...) are based on the human factor for ensuring the interior comfort indicators. For the energy efficient buildings, passive type, the comfort is an issue that should be viewed differently from standard type buildings.

Future buildings will be, in large part, smart buildings with smart tire, dynamic- adaptable so that they can adapt to the dynamic characteristics of the external climate and to the demands of users. In these buildings the comfort is characterized himself, by dynamism and, as such, the criteria for determining its parameters are different in the cases listed above.

Among the criteria above, thermal criteria are of major importance in terms of design and performance evaluation of heating, cooling, ventilation, and air conditioning.

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The parameters that can influence comfort can be grouped the three major classes (Markus & Morris, 1980): a. The physical parameters (air temperature, mean radiant temperature of the walls of the enclosure, relative air humidity, velocity relative air into the enclosure; atmospheric pressure; light intensity, noise); b. organic parameters (age, sex, national characteristics of occupants); c. external parameters (level of human activity, type of clothing, social conditions).

The biggest influence on thermal comfort have: temperature, relative humidity, barometric pressure and air velocity and clothing and human work activities. Positive or negative effect of a parameter can be improved or offset by another parameter.

For design the NZEB building is important to establish the thermal comfort parameters, such that, it is obtained for a minimum consumption of energy.

To this end, they proposed different models of hygro-thermal comfort (or only heat), each of which is correlated with the requirements imposed buildings for that era. *Hygro-thermal comfort models* are very important for designing energy efficient buildings. They describe the quantitative limit climatic conditions for which people feel good in terms of heat. These conditions serve to ensure a comfortable thermal environments with minimal energy consumption, regardless of outside weather conditions.

The importance of a comfortable interior climate, while the outdoor climate parameters vary over time, simultaneously with "avoiding unnecessary use of energy" are among the declared objectives of the European Directive of buildings energy performance.

There are several models for comfort (Cotorobai *et al.*, 2009), of which are dominant and fit for energy purpose:

a) *The Predicted Mean Vote (PMV)*, which is based on the proposed and reasoned model by Fanger;

b) **Adaptive Comfort model**, which takes into account the adaptive capacity of the occupants of a building at the seasonal climate variations and its location/climate zone.

Each of the mentioned models has certain particularities, which their is recommended in some design conditions and equipping of buildings, respectively, for buildings that ensure comfort in summer is achieved by:

i) Active systems: The Predicted Mean Vote (PMV);

ii) Passive: The Adaptive Comfort;

iii) Mixed systems: both models.

The two models mentioned above differ between them by the mod of consideration the resultant temperature of indoor comfort, and respectively, by mod of consider the operative confort temperature in the warm period, when comfort can be provided with active or passive systems.

Designing systems for buildings and related facilities and to assess the energy performance of their comfort models were formalized in order to establish ranges of parameter values hygro-thermal comfort inside (design and energy performance assessment).

To characterize the comfort hygrothermal, both buildings in relation to this criterion, defined a set of global indicators comfort (*Predicted Mean Vote/PMV, Predicted Percent of dissatisfied/PPD; Temperature operative/To*) (ASHRAE Standard 55-1992, 2004; ISO 7730:2007; EN 15251: 2007). Rules relating to interior comfort have a narrower scope (SR EN 7730) or larger (SR EN 15251; ASHRAE 55).

2. Research Objectives

Imposition of new energy requirements for future buildings (buildings NZBE) requires the revision of these rules, adapt to new requirements and that their improvement.

Under the European directive to increase the energy performance of buildings has established itself providing new demands of quality energy, differentiated according to age buildings (new, existing) and time horizon (short (2020), Long (2050)). In the short term, new buildings will have to meet requirements NZBE buildings and, in the long term and existing buildings requires bringing the same quality requirements as those imposed on new buildings.

But the performances qualified attribute NZBE building are set by individual states and therefore they are different from state to state.

Under these circumstances it can meet NZBE building for proposing hyper- insulation and hyper- sealing.

Hyper-sealing requires aeration controlled or active systems that can affect the heat balance of buildings during summer. On the other hand, the buildings once designed and should provide comfort hygrothermal summer and in winter by appropriate control strategies provided for its purchase.

In the context of climate change and respectively in the manifestation periods sultry increasingly longer and of climatic differences Winter-Summer increasingly larger, the buildings hyper-insulated and hyper-tight designed for comfort during winter with minimum energy resources, may require energy resources relatively high for the comfort during the summer.

The paper presents an analysis of the impact of summer climate variations on comfort indicators in buildings NZBE, evaluating them according to SR EN 15251 and ASHRAE Standards-55. The analysis aims to highlight the dynamics comfort indicators in real operating conditions different from those

considered in the design process, and identify appropriate control strategies.

To this end will be assessed:

a) indicators of comfort for the summer period, for a residential building that was purchased Hygrothermal comfort with passive cooling strategies designed in accordance with EN 12051 SR: 2007;

b) indicators comfort in hot climates during the summer, for the same building in order to identify the impact of these conditions on comfort category, respectively.

3. Research Results

3.1. Working Assumptions

In SR EN 12521: 2007 for residential buildings are set limits variation indicators comfort and calculation parameters for design in relation to quality classes, the means to provide comfort (active, mechanical/liabilities) and seasons climate. Recommended levels of indoor temperatures used in the design of residential buildings and related HVAC systems are shown in Table 1.

Table 1

Operational Temperature Values for Homes with Different Levels of Comfort (extracted from EN 12521)

	Category	Operational temperature				
Building type	of comfort	The minimum (for heating -Winter)	The maximum (cooling-Summer)			
Rooms in residential buildings	Ι	21.0	26.0			
Sedentary: $M = \sim 1.2$ met;	II	20.0	26.5			
Clothing: ~1.0 clo	III	18.0	27.0			

In Romania, but not only, over 50% of existing residential buildings are made in periods with much lower energy quality requirements in rapport with NZBE buildings, and, a large part of them will undergo modernization process. Packages of measures for renovation/modernization of existing buildings thermal recommended to use low-e windows. The paper presents an extract from an analysis of the impact of climate variations on maintaining comfort in existing residential buildings modernized or undergoing modernization, and for a building equipped with low-e windows.

For evaluating the radiation dosimetry, we analysed the behaviour of a triple windows with low-e glass in the simulation software Window 7 and I retained, for summer weather conditions, according to NFRC standard 100-200 (Te = 32° C) the

temperature the inner surface of the window ($Tsi = 33.3^{\circ}C$) (Fig. 1).

Note: (In recent years, in Romania, outside air temperature value exceeded for periods longer than 30 days Tae value = 32° C, reaching extremes of Tae = 39° C.

		Lay	er 1	Lay	er 2	Lay		
	Outside air	Outer Inner		Outer	Inner	Outer	Inner	Inside air
		surface	surface	surface	surface	surface	surface	
U _{factor}	-18.0	-16.2	-15.9	3.7	3.8	13.0	13.2	21.0
SHGC	32	46.3	47.2	40.4	40.3	33.5	33.3	24.0

Fig. 1 – Air temperature, in different cross sections of the window, under standard NFRC 100-200 conditions, in the winter and the summer (Screen capture Windows 7).

The building model was made in TRNSYS and was simulated its behaviour under dynamic climate conditions of Iaşi. The simulation results on surface temperatures on the inside of the windows revealed in extreme conditions and values Tsi = 39.3°C.

The radiant average temperature resulting from the room behavior analysis is:

a. for the standard climate conditions calculation *NFRC 100-200*: T_{MR} , s = 28.4°C;

b. in the extremal summer conditions: $T_{MR,s} = 30.4$ °C

The analysis covered:

- to the establishment the indicators of comfort, in accordance with SR EN 12521 and ASHRAE-55, by method PMV and method of adaptive comfort, for the operation temperature indicated for the design of the residential buildings in category I and III (Table 1), with the parameters of indoor environment and the standardized parameters related to human metabolism for the summer period and for residential buildings;
- to the establishment the indicators of comfort, in accordance with Standard SR EN 12521 and ASHRAE-55, by PMV and Adaptive comfort method, for the operation temperature indicated for the design of the residential buildings in category I and III (Table 1), with the parameters of indoor environment and the standardized parameters related to human metabolism for the summer period residential buildings and for radiant average temperature in extreme conditions.

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Comparative analysis. Psychrometers graphics PMV Method: ASHRAE-55 I. Indoor environment parameters Human parameters Air temperature 26 Metabolic rate Rn met 1.1 °C Mean radiant 28.3 Clothing level (Thypical summer indoor clo 0.5 Т., ^{0}C N 0.1 Air speed m/s Humidity 50 % PMV [%] 0.57 tob rh Wa two top 25.9 49.2 10.3 18.5 14.3 76 2 a)Psychometric chart (air temperature) PPD [%] 12 Sensation Slightly Warm Set 15 Does not comply with ASHRAE Standard 55-2013* Note: The abscissa is the dry-bulb temperature, and the mean radiant temperature (MRT) is fixed.. Each point on the chart has the same MRT, which defines the comfort zone boundary. In this way it can see how changes in MRT affect thermal 20 20 22 24 26 Drybulb Temperature [* perature [*C] comfort, yet each point will have the same MRT 26.0 °C 51.1 % 10.7 g w/kg 18.9 °C 15.0 °C 27.4 kJ/kg PMV [%] 0.20 teo rh Wa two teo h PPD [%] 6 (ob)perative temperature) Psychometric chart Sensation Neutral /kg_{da}] 25.7 Set Complies with ASHRAE Standard 55-2013 Note: The abscissa is the operative temperature and for each point dry-bulb temperature equals mean radiant temperature (DBT = MRT). The comfort zone represents the combination of conditions with the same DBT and MRT for which the PMV is between 10 12 22 20 24 26 28 0.5 and +0.5, according to the standard. PMV [%] 0.5 Relative umidity cart PPD [%] 12 Sensation Slightly Warm c)Temperature Set SHRAE Doe Note: This chart represents only two variables, dry-bulb temperature and relative humidity. The PMV calculation are still based on all the psychrometric variables, but the visualization becomes easier to understand PMV [%] 0.2PPD [%] 1.0 0.9 0.8 operative temperature Sensation Neutral Set 25.7 d)Air speed-<u>الم</u> Complies with ASHRAE Standard 55-2013 ¥ 0.6 Note: This chart represents air speed against operative 0.4 temperature. The operative temperature for each point is determined by dry-bulb temperature equals mean radiant 0.2 temperature (DBT = MRT). The calculation of PMV comfort 0.1 zone is based on all the psychrometric variables, with PMV 24 Or 26 28 ve Temperature [°C] values between -0.5 and +0.5 according to the standard. * Each point on the graph is the same T_{mr}, within the limits of the comfort zone. ** Comfort zone: the combination of circumstances, the same T_{bu} and T_{mr} for which PMV $\in [-0.5; 0.5]$ (as standard). Note: Indicators comfort set for regulated interior comfort parameters not remains constants in different functional external conditions; operating point is established outside the comfort zone

Table 2

						uation)						
			١.		/ Met	hod: SR EN 15251						
	Indoor enviro						parameters	_				
	nperature		<u>'C</u>	26		Metabolic rate		R _m	met	1.1		
	adiant	m	°C	28.3		Clothing level (Thypical sum	mer indoor	$N_{\hat{i}}$	clo	0.5		
Air spe		a	m/s %	0.1 50								
Humid	5	φ	%	50	- 30	DN 4) / [0/]		0.7				
	tab 26.0 °C nh 51.1 %			///	- 50	PMV [%] PPD [%]		0.7 55				
	Wa 10.7 g w/kg da two 18.9 °C		/	///	25	Category		55 IV				
Ħ o	tdp 15.0 °C h 27.4 kJ/kg		//		[e	Does not comply v	with SR EN		1 *			
a)Psychometric chart (air temperature)	10 12 14 16 18 20 Dry	22 24 2 -bulb Temperatur		30 32 34 30	10 I	Note: The abscissa is the d the mean radiant temperat point on the chart has the s the comfort zone boundary changes in MRT affect ther will have the same MRT	ry-bulb ten ure (MRT) same MRT, . In this wa	ipera is fixe whic y it c	ture, d ed Ed h defin an see	ach nes how		
		hart (operative to) *		PMV [%]		0.2				
					- 30	PPD [%]		6				
	rh 51.2 %			///	50	Catgory I						
lre	Ws 10.7 g w/k g ds two 18.7 °C tdo 14.9 °C		/	///	25	Complies with ASHRAE S	standard 55	-2013	3			
b)Psychometric chart (operative temperatture	10 12 14 16 18 20 Op			30 32 34 30	idity Ra	Note: The abscissa is the for each point dry-bulb radiant temperature (DBT represents the combinati same DBT and MRT for w 0.5 and +0.5, according to	temperatu = MRT). T on of con which the P	re e The c dition MV i	quals omfor 1s wit	mean t zone th the		
	100		0	v		PMV [%]		0.57				
lity	90					PPD [%]		12				
mic	80					Category		III				
c)Temperature –Relative umidity cart			Temperatu	6 28 30 32 лю [*C]	2 34	Set Note: This chart represents temperature and relative hu are still based on all the ps visualization becomes easier	midity. The ychrometric to understan	PMV varia d	' calcu ubles, i	lations but the		
			0			fort parameters not remains ished outside the comfort z		in di	fferent	t		

Table 2

		Comp	<i>arative</i> a Pl	analysis. Ps MV Method:	<i>ychrometers gr</i> ASHRAF-55	aphics				
	Indoor environ	ment p			1	Human parar	neters			
Air tem	perature	ta	⁰ C	27	Metabolic rate R _m me					
	adiant temperature	T _{mr}	⁰ C	30.4	Clothing level summer indoor		Nî	clo	0.5	
Air spe		Va	m/s	0.1						
Humidi	ty	φ	%	50						
Psychometric chart (air temperature)	tas 27.0 °C n' 52.4 % W 11.7 guikgas tas 19.9 °C tas 19.9 °C h 29.8 kJkg			- 30 - 25 - 20 - 15 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	PMV [%] PPD [%] Sensation	1.09 30 Slightly Warm				
Psychor (air ten	10 12 14 16 18 20 Dry	22 24 bulb Temper	26 28 30 ature [°C]	-5	Set	28.6 Does not comply with ASHRA Standard 55-2013*				
	teb 27.0 °C			/ /Γ ³⁰	PMV [%]		1.09			
	rh 51.6 % ₩a 11.5 gw/kgda		/		PPD [%]	30				
(e)	two 19.8 °C tep 16.0 °C			- 25	Sensation	Sli	ghtly W	arm		
nart utu	h 29.4 kJ/kg			20 [49]	Set		28.6			
Psychometric chart (operative temperature)		22 24 arative Temper	26 28 30 ature [*C]	20 ^{(hg}) (hg) (hg) (hg) (hg) (hg) (hg) (hg) (hg		Does not co Stan	dard 55-2		RAE	
	100				PMV [%]		1.09			
•	90				PPD [%]		30			
tive	80				Sensation	Sli	ghtly W	arm		
Temperature –Relative humidity cart	Ibit 60 50 - 50 - 30 - 10 - 0 - 0 -		24 26 28 emperature [°C]	30 32 34 36	Set		ndard 55-	2013		
zone: t standa	n point on the graph the combination of rd). Indicators comfort	is the circur	e same T nstance	s, the same T	$_{bu}$ and T_{mr} for w	which PMV	∈ [-0.5	; 0.5]	(as	

Table 3 Comparative analysis. Psychrometers gr

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				Continu					
	<u> </u>				SR EN 12521				
	Indoor environ						arameters		
Air tempe Mean rad	ant temperature	t _a T _{mr}	⁰ C ⁰ C	27 30.4	Metabolic rate Clothing level summer indoor	(Typical	R _m N _î	met clo Clo 0 0 0,7 <p< td=""> 0</p<>	1.1 0.5
Air speed		Va	m/s	0.1	Summer massi	(ciouning)			
Humidity		φ	%	50					
tab	27.1 °C		/	/ / [30	PMV [%]		1.09		
rh Wa two	51.0 % 11.5 gw/kgda 19.8 °C			-25		Cat. I	Cat. II	С	at. III
Psychometric chart	16.0 °C 29.3 kJ/kg			20 rep _{6y/} M		- 0,2 <pm V<+0,2</pm 	- 0,5 <pmv< +0,5</pmv< 		- :PMV< 0,7
etric			//	10 Horizon (10 March 10 March	PPD [%]		30		
hom			0	10 H		<6	<10		<15
SVC		H		_	Category				IV
	12 14 16 18 20 2	2 24 26	28 30 32	- 5 - 0 34 36		Does not	comply with	th EN-1	5251
tas rh	Dry-bulk 26.9 °C 52.0 %) Temperature		/ / [30	PMV [%]		0.53		
Wa two top	11.5 g w/kg da 19.8 °C 16.1 °C			-25		Cat. I	Cat. II	С	at. III
Psychometric chart	29.5 kJ/kg			10 10 10 10 10 10		- 0,2 <pm V<+0,2</pm 	- 0,5 <pmv< +0,5</pmv< 		- :PMV< 0,7
netric				Ity Ratio	PPD [%]		11		
vchor		1	0	10 III		<6	<10		<15
Sd		#		- 5	Category			III	
10		2 24 20 ve Temperatu		2 34 36					
-	00				PMV [%]		1.09		
fv ca	90					Cat. I	Cat. II	C	at. III
Temperature – Kelative humidity cart Relative hundity [8]	70 60 50		•			- 0,2 <pm V<+0,2</pm 	- 0,5 <pmv< +0,5</pmv< 		- :PMV< 0,7
-Relative h Relative Humidity [%]	40				PPD [%]		30		
srature – _{Re}	30					<6	<10	•	<15
emne	10 0 10 12 14 16 18 2	20 22 24	26 28 30	32 34 36	Category				IV
		Dry-bulb Temp				Does no	t comply w	ith EN-	15251

Table 3Continuation

				daptive chart				
		a.	Adap	tive method: ASHRA	E-55			
Indoor environmen	nt parar	10			Human parameters		-	
Air temperature	ta	°C	26	Metabolic rate		R _m	met	1.1-1.3
Mean radiant temperature	T _{mr}	^{0}C		Clothing level (Typical st	ummer indoor	$N_{\hat{i}}$	clo	0.5-1.0
Air speed	Va	m/s	0.3					
Prevailing mean outdoor	T _{m_ae}	⁰ C	33.5		1			
34				acceptability limits: 80%	Operative temperature	: 24.7-3	81.7 ℃	
			Θ	\Rightarrow Status	Comfortable			
ive c				90% acceptability limits	Operative temperatu	re: 25.7	7-30.7 °C	C
dapti operative 7 25 25 25					Comfortable			
18 18 16 14 10 12 14 16 18 20 Prevailing Mean Ou Prevailing Mean Ou Prevailing Mean Ou Prevailing Mean Ou	22 24 2	16 28 3	0 32	\Rightarrow Status	Complies with ASH	RAE S	tandard	55-2013
Indoor environmen					Human parameters			
Air temperature	t _a	¹⁰ C	27	Metabolic rate	numan parameters	R _m	met	1.1-1.3
Mean radiant temperature	T _{mr}	°C	28.3	Clothing level (Typical s			clo	0.5-1.0
Air speed	V _a	m/s	0.3	Clouing lever (Typicar s		1 1	cio	0.5 1.0
Prevailing mean outdoor	T _{m_ae}	⁰ C	33.5					
34	ac	L		80% acceptability limits	Operative temperatu	re: 24.7	to 31.7	°C
32	32 30 28			\Rightarrow Status	Comfortable			
30 30 30				90% acceptability limits	Operative temperature: 25.7 to 30.7 °C			
Adaptive chart	22 24 2 Jultor Temperat	6 28 30	32	⇒ Status	Comfortable Complies with ASH	RAE S	tandard	55-2013
Indoor environmen					Human parameters			
Air temperature	ta	⁰ C	27					1.1-1.3
Mean radiant temperature	T _{mr}	°C	30.4	Clothing level (Typical st clothing)	Nî	clo	0.5-1.0	
Air speed	Va	m/s	0.3					
Prevailing mean outdoor	T _{m_ae}	⁰ C	33.5					
34				80% acceptability limits	Operative temperatu	re: 24.7	to 31.7	′℃
32				⇒ Status 90% acceptability limits	Comfortable			
+ 30	30				Operative temperatu	re: 25.7	to 30.7	°C
C 28	28			\Rightarrow Status	Comfortable			
C 26	A Constraint of the second sec				Complies with ASH	RAES	tandard	55-2013
Adaptiv	2 24 26	28 30	32					

ng e

(a) There is no mechanical cooling system installed. No heating system is in operation;
(b) Metabolic rates ranging from 1.0 to 1.3 met; and
(c) Occupants are free to adapt their clothing to the indoor and/or outdoor thermal conditions within a range at least as wide as 0.5-1.0 clo.

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				Table 4							
		b.		ptive method: SR EN 12							
Indoor environmen	t parai			Human parameters							
Air temperature	ta	⁰ C	26	Metabolic rate		R _m	met	1.1-1.3			
Mean radiant temperature	T _{mr}	⁰ C	28.3	Clothing level		Nî	clo	adaptable			
Air speed	Va	m/s	0.3								
Prevailing mean outdoor	T _{m_ae}	⁰ C	30		1						
30				Acceptability limits: Class III	Operative tempera	ature: 2	24.7 to	33.5 °C			
32		and a		Status	Comfortable						
			e	Class II acceptability limits	Operative tempe	rature	: 25.7	to 32.5 °C			
22 Produce de la composición d				Status	Comfortable						
20 000 (qab)				Class I acceptability limits	Operative tempe	rature	: 26.7	to 31.5 °C			
				Status	Comfortable						
Outdoor Running h	20 22 24 dean Temperature	rci 20	30		C	ompli	es with	EN-1525			
Indoor environmen	t parai	meter	S	Hu	man parameters						
Air temperature	ta	^{0}C	27	Metabolic rate		R _m	met	1.1-1.3			
Mean radiant temperature	T _{mr}	^{0}C	28.3	Clothing level		Nî	clo	adaptable			
Air speed	Va	m/s	0.3								
Prevailing mean outdoor	T_{m_ae}	^{0}C	30								
36				Class III acceptability limits	Operative tempe	rature	: 24.7	to 33.5 °C			
32		1		Status	Comfortable						
c char			Ģ	Class II acceptability limits	rature	: 25.7	to 32.5 °C				
				Status	Comfortable						
Adaptive chart	1			Class I acceptability limits	Operative tempe	rature	: 26.7	to 31.5 °C			
18				Status	Comfortable						
14 10 12 14 16 18 Outdoor Running I	20 22 Mean Temperati	24 26 ure [°C]	28 30		C	ompli	es with	EN-1525			
Indoor environmen	t parar	meter	S	Hu	man parameters						
Air temperature	t _a	^{0}C	27	Metabolic rate		R _m	met	1.1-1.3			
Mean radiant temperature	T _{mr}	^{0}C	30.4	Clothing level		Nî	clo	adaptable			
Air speed	va	m/s	0.3								
Prevailing mean outdoor	T_{m_ae}	⁰ C	30		1						
34				Class III acceptability limits	Operative tempe	rature	: 24.7	to 33.5 °C			
			e		Comfortable						
Adaptive chart				Class II acceptability limits		rature	: 25.7	to 32.5 °C			
apti					Comfortable		267				
C 20 18					Operative tempe	rature	: 20.7	to 31.5 °C			
16 14 10 12 14 16 18 Outdoor Running h	20 22 24	4 26 28	30	Status	<i>Comfortable</i>	ompli	es with	EN-1525			
Note: Method is applicable of											

windows and occupants may freely adapt their clothing to the indoor an spaces are the following:
(a) There is no mechanical cooling or heating system in operation;
(b) Metabolic rates ranging from 1.0 to 1.3 met;
c) Occupants are allowed to freely adapt their clothing insulation.

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3.2. Research Results

The results are presented in Tables 2, ..., 4. Are represented:

- Psychrometers graphs $t_a = f(T_{Tbu}) T_o = f(T_{Tbu})$, and $\phi = f(T_{Tbu})$ and comfort zones in standard climatic conditions and extreme weather conditions in summer, conformement:
 - the PMV method for standard ASHRAE 55 and (Tables 2a and 3a);
 - EN 12051 (Tables 2b and 3b).
- Adaptive diagrams obtained using adaptive comfort method, established under the same rules and that the same conditions (Table 4).

4. Discussion.

The analysis of diagrams can be drawn the following conclusions:

1° Design of the housing building with active systems to ensure comfort parameters indicated in the rules EN 12521 and ASHRAE-55, in accord with the PMV method does not guarantee maintaining an indoor environment comfortable, in climate conditions much different from those considered in the design, in the absence of control strategies effective internal parameters (Tables 2 and 3).

2° Design of the housing building according with the two rules by using method "adaptive comfort" and by considering only strategies passive ensuring hygro-thermal comfort during the summer ensure the maintaining a comfortable atmosphere and under periods hot (Table 4).

There are different passive strategies for the control of the hygrothermal indicators/parameters of the comfort (Fig. 2) for the cold and the warm sezon. But these strategies must be carefully balanced with quality assurance strategies indoor air. In the climatic conditions of Romania, to ensuring Hygrothermal comfort during winter is necessary the use of active systems.

5. Conclusions

Hygro-thermal comfort parameters for design of buildings NZBE, in the climatic zones with large variations of temperature winter-summer and with the sultry important periods, must consider differently, for the winter period, the warm period and the hot periods. The strategies comfort control must be correlate to specific of each climatic periods.

Maintaining comfort indicators considered in the design of buildings NZBE lifespan can be provided if designed:

a) after standard passive buildings to operate in winter but with appropriate technologies that favour the reduction of inputs sun in summer.

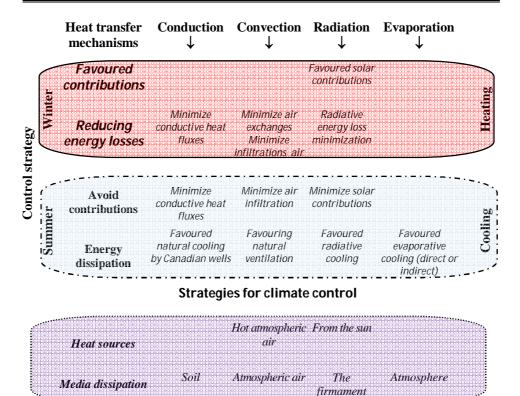


Fig. 2 – Hygrothermal comfort control strategies.

Are possible such technologies: heliotrope or thermotropic glass windows showing the possibility of controlling thermal and optical radiation transmitted to and from the interior and exploitation of solar radiation in excess of the requirements to ensure visual comfort and indoor environment; south wall cladding with glass bricks intelligent, dynamically adaptive radiation and solar thermal devices; north wall cladding panels finishing with thermo-active; use possible strategies coupled with the ground elements to increase the thermal inertia and thermoregulation (MSF), ...

b) after standard passive buildings during the summer but punctual provision of indoor climate control strategies for hot periods (natural ventilation strategy) ...

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CONSIDERAȚII ASUPRA INDICATORILOR DE CONFORT DIN CLĂDIRILE CU CONSUM REDUS DE ENERGIE ÎN REGIM DINAMIC

(Rezumat)

Impunerea noilor exigențe energetice pentru clădirile viitorului necesită revizuirea tuturor normelor referitoare la parametrii de proiectare ai acestora. Normele referitoare la confortul higro-termic al clădirilor pot avea un impact important asupra consumului de energie în exploatare. Adaptarea acestora la noile exigențe impuse clădirilor și previzionarea unui comportament al clădirilor cât mai aproape de cel real este absolut necesară în acest context. Pe de altă parte, strategiile de asigurare a confortului în aceste clădiri trebuiesc atent analizate și corect considerate în cadrul normelor deoarece confortul higro-termic este influențat de climatul exterior, performanțele clădirii și exigențele utilizatorilor. În cadrul lucrării se prezintă o analiză a impactului variațiilor climatice estivale asupra indicatorilor de confort din clădirile NZBE, prin evaluarea acestora conform normelor EN 15251 și ASHRAE -55. Analiza vizează evidențierea dinamicii indicatorilor de confort în condițiile reale de funcționare și identificarea unor strategii de control.